

## Supplemental Material for:

### Formation criterion for binary metal diboride solid solutions established through combinatorial methods

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**Table S1.** Calculated lattice parameters ( $a$  and  $c$ ) and energies ( $E$ ) of  $(M_xN_{1-x})B_2$  solid solutions ( $M, N = \text{Hf, Zr, Ta, Nb, or Ti}$ ).

No.	$(M_xN_{1-x})B_2$	$a$ (Å)	$c$ (Å)	$E$ (eV/atom)
1	$(\text{Ta}_{0.5}\text{Ti}_{0.5})B_2$	3.069	3.273	-8.632
2	$(\text{Nb}_{0.5}\text{Ti}_{0.5})B_2$	3.073	3.273	-8.391
3	$(\text{Zr}_{0.5}\text{Ta}_{0.5})B_2$	3.134	3.427	-8.699
4	$(\text{Hf}_{0.5}\text{Ta}_{0.5})B_2$	3.120	3.401	-8.935
5	$(\text{Ta}_{0.5}\text{Nb}_{0.5})B_2$	3.106	3.321	-8.835
6	$(\text{Hf}_{0.5}\text{Zr}_{0.5})B_2$	3.156	3.518	-8.564
7	$(\text{Hf}_{0.5}\text{Nb}_{0.5})B_2$	3.126	3.402	-8.703
8	$(\text{Zr}_{0.5}\text{Nb}_{0.5})B_2$	3.140	3.429	-8.465
9	$(\text{Hf}_{0.5}\text{Ti}_{0.5})B_2$	3.096	3.361	-8.448
10	$(\text{Zr}_{0.5}\text{Ti}_{0.5})B_2$	3.112	3.390	-8.196
11	$(\text{Hf}_{0.9}\text{Ta}_{0.1})B_2$	3.138	3.469	-8.830
12	$(\text{Hf}_{0.9}\text{Nb}_{0.1})B_2$	3.139	3.468	-8.782
13	$(\text{Nb}_{0.9}\text{Ti}_{0.1})B_2$	3.102	3.311	-8.566
14	$(\text{Nb}_{0.8}\text{Ti}_{0.2})B_2$	3.096	3.302	-8.524
15	$(\text{Nb}_{0.7}\text{Ti}_{0.3})B_2$	3.088	3.293	-8.481

16	(Ta <sub>0.8</sub> Ti <sub>0.2</sub> )B <sub>2</sub>	3.090	3.304	-8.891
17	(Ta <sub>0.6</sub> Ti <sub>0.4</sub> )B <sub>2</sub>	3.076	3.284	-8.720
18	(Hf <sub>0.1</sub> Ta <sub>0.9</sub> )B <sub>2</sub>	3.106	3.338	-9.030
19	(Hf <sub>0.1</sub> Nb <sub>0.9</sub> )B <sub>2</sub>	3.112	3.337	-8.628
20	(Nb <sub>0.1</sub> Ti <sub>0.9</sub> )B <sub>2</sub>	3.042	3.232	-8.197
21	(Ta <sub>0.2</sub> Ti <sub>0.8</sub> )B <sub>2</sub>	3.048	3.243	-8.349
22	(Ta <sub>0.4</sub> Ti <sub>0.6</sub> )B <sub>2</sub>	3.062	3.263	-8.540

**Table S2.** The leave-one-out cross validation accuracy of the model and the value of  $\theta_0$  -  $\theta_4$  when different training data was used (only 1 validation data was used and the rest was used as training data).

No.	Validation data	$\theta_0$	$\theta_1$	$\theta_2$	$\theta_3$	$\theta_4$	Accuracy
1	(Ta <sub>0.5</sub> Ti <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
2	(Nb <sub>0.5</sub> Ti <sub>0.5</sub> )B <sub>2</sub>	56.365	-82.185	-156.837	8.729	11.446	100%
3	(Zr <sub>0.5</sub> Ta <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
4	(Hf <sub>0.5</sub> Ta <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
5	(Ta <sub>0.5</sub> Nb <sub>0.5</sub> )B <sub>2</sub>	139.830	-219.434	-443.647	49.402	25.569	100%
6	(Hf <sub>0.5</sub> Zr <sub>0.5</sub> )B <sub>2</sub>	55.544	-81.578	-158.255	10.386	10.949	100%

7	(Hf <sub>0.5</sub> Nb <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
8	(Zr <sub>0.5</sub> Nb <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
9	(Hf <sub>0.5</sub> Ti <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
10	(Zr <sub>0.5</sub> Ti <sub>0.5</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
11	(Hf <sub>0.9</sub> Ta <sub>0.1</sub> )B <sub>2</sub>	56.123	-81.766	-157.268	9.168	11.235	100%
12	(Hf <sub>0.9</sub> Nb <sub>0.1</sub> )B <sub>2</sub>	56.055	-81.757	-157.373	9.303	11.212	100%
13	(Nb <sub>0.9</sub> Ti <sub>0.1</sub> )B <sub>2</sub>	56.053	-81.750	-157.381	9.311	11.207	100%
14	(Nb <sub>0.8</sub> Ti <sub>0.2</sub> )B <sub>2</sub>	60.561	-84.631	-152.915	1.498	10.180	<b>0%</b>
15	(Nb <sub>0.7</sub> Ti <sub>0.3</sub> )B <sub>2</sub>	56.502	-84.096	-152.517	7.374	12.884	100%
16	(Ta <sub>0.8</sub> Ti <sub>0.2</sub> )B <sub>2</sub>	56.052	-81.756	-157.378	9.309	11.210	100%
17	(Ta <sub>0.6</sub> Ti <sub>0.4</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
18	(Hf <sub>0.1</sub> Ta <sub>0.9</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
19	(Hf <sub>0.1</sub> Nb <sub>0.9</sub> )B <sub>2</sub>	56.053	-81.747	-157.377	9.309	11.206	100%
20	(Nb <sub>0.1</sub> Ti <sub>0.9</sub> )B <sub>2</sub>	65.640	-77.226	-158.810	12.648	-2.401	<b>0%</b>
21	(Ta <sub>0.2</sub> Ti <sub>0.8</sub> )B <sub>2</sub>	55.052	-81.344	-156.839	8.964	12.262	100%
22	(Ta <sub>0.4</sub> Ti <sub>0.6</sub> )B <sub>2</sub>	55.630	-81.668	-157.024	9.047	11.763	100%

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